

LAMPIRAN A
SPESIFIKASI ALAT

A. Ruang Bakar

Tabel 11. Spesifikasi Ruang Bakar

Dimensi	Ukuran
Bentuk	Box
Panjang	100 cm
Lebar	58 cm
Tinggi	70 cm

B. Longitudinal Water Tuber Boiler

Tabel 12. Spesifikasi WaterTube Boiler

Dimensi	Ukuran
Panjang boiler	100 cm
Diameter boiler	30 cm
Diameter tube	2,5 cm
Panjang tube	70 cm
Tebal tube	0,15cm
Jumlah tube	16 buah

C. Turbin

Tabel 13. Spesifikasi Turbin

Dimensi	Ukuran
Bentuk	Silinder sirip
Diameter	51 cm
Tebal	0,6 cm
Jumlah sudu	54 buah
Jarak dari poros	25 cm
Tebal turbin	5 cm
Luas turbin	0.52 m ²

D. Generator

Tabel 14. Spesifikasi Generator

Dimensi	Ukuran
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Daya	3000 watt
NP	3000 rpm
Frekuensi	50/60 Hz
Phase	1
voltase	220
Mas ampere	13.6
Cos α	1

E. Kondensor

Tabel 15. Spesifikasi Kondensor

Dimensi	Ukuran
Bentuk	Persegi panjang
Panjang	79 cm
Lebar	61 cm
Tinggi	35 cm
Diameter <i>tube</i>	0,5 in
Jumlah <i>tube</i>	16 buah

F. Kompresor

Tabel 16. Spesifikasi Kompresor

Dimensi	Ukuran
Bentuk	Silinder vertikal
Diameter selang	1,5 cm
Tinggi	39 cm
Luas penampang	2024 cm ²
Diameter tangki	14 cm
Tenaga	1 HP
Tekanan maksimum	8 Bar
Volume	8 Liter
Putaran	2850 rpm
Kapasitas	150 Liter/menit

G. OilTank

Tabel 17. Spesifikasi OilTank

Dimensi	Ukuran
Bentuk	Silinder
Diameter	27 cm
Panjang	46 cm
Tebal	4 mm

H. Pompa**Tabel 18. Spesifikasi Pompa**

Dimensi	Ukuran
Tinggi <i>boiler</i>	75 cm
Diameter <i>boiler</i>	50 cm
Diameter <i>tube</i>	2,5 cm
Panjang <i>tube</i>	75 cm
Tebal <i>tube</i>	0,15 cm
Jumlah <i>tube</i>	9 buah
Tenaga	2,2 HP
Daya	1,6 KW
Putaran	2800 rpm
Tegangan	220 V
Arus	8,5 A

**LAMPIRAN B
DOKUMENTASI KEGIATAN**







LAMPIRAN C
GAMBAR ALAT



Gambar21. Steam Drum



Gambar 22. Longitudinal Tubesheet



Gambar23. Tubesheet Superheater



Gambar24. Furnace



Gambar 25. Kompresor



Gambar 26. Tangki Bahan Bakar



Gambar 27. Sudu Turbin



Gambar 28. Kondensor



Gambar 30. Level Volume



Gambar 29. Pompa



Gambar31.kontrolPanel



Gambar 32. Generator



Gambar 33. Burner



Gambar 34. Open Pulley Sistem



Gambar 35. Temperature Gauge



Gambar 36. PressureGauge



Gambar 37. *Flowmeter*



Gambar 38. *Water Tank*

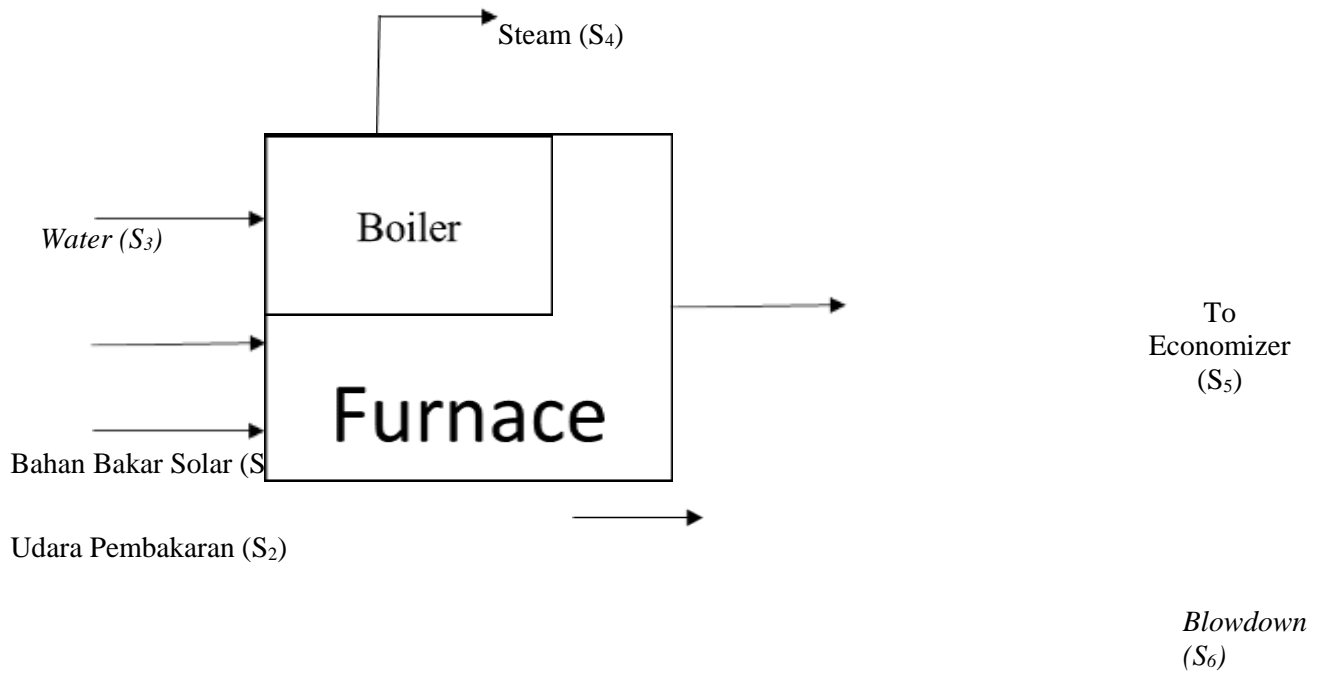


Gambar 39. *Tubesheet Economizer*



Gambar 40. Prototipe *Steam Power Generator* Keseluruhan

LAMPIRAN D
DATA PENGAMATAN



Tabel.19 laju alir Bahan Bakar

Tekanan (bar)	Area Operasi	Flow Bahan Bakar (kg/jam)
5	Liquid Burner	2,000
10	Liquid Burner	1,750

Tabel.20 laju alir Steam

Tekanan (bar)	Area Operasi	Flow Steam (kg/jam)
45	Drum	15
30	Drum	10

Tabel.21 laju alir Blowdown

Tekanan (bar)	Area Operasi	Flow Blowdown (kg/jam)
45	Drum	15
30	Drum	20

Tabel.22 Data proses Steam Power Plant

Parameter	Tekanan	
	10	5
Temperatur Bahan Bakar (°C)	30	30
Temperatur Udara (°C)	30	30
Temperatur Wall Furnace (°C)	152	150

Temperatur Flue Gas (°C)	221	219
Tekanan steam (bar)	10	5
Temperatur Blowdown (°C)	100	100
Temperatur BFW (°C)	28	28
AFR		16:01

LAMPIRAN E
PERHITUNGAN
Neraca Massa Water Tube Boiler

Pada *Water Tube Boiler* terjadi proses produksi uap yang kemudian akan dimanfaatkan sebagai penggerak Turbin untuk menghasilkan listrik sebesar 1 kw.

Basis 1 jam operasi

Flow solar 2,00 L

Massa solar	1,75	kg
HHV	10500	kcal/kg
spgr	0,874	kg/L

Spesifikasi Burner

Diameter	6,4 cm	r =	3,2 cm
Luas penampang burner	=	$2 \cdot 3,14 \cdot r^2$	
	=	64,3072	cm ²
	=	0,00643072	m ²
Kecepatan aliran	=	0,761	m/s
Laju alir massa	=	17,61760051	m ³
-Massa Udara dari air kompresor	=	28,00	kg
Mol udara suplai	=	$\frac{28,00 \text{ kg}}{28,84}$	
	=	0,9709	kmol

Tabel. 23 Analisis Orsat
Flue gas

Komponen	% vol
CO ₂	8,48%
CO	2,13%
O ₂	7,15%
N ₂	82,24%
Total	100,00%

-AFR Pembakaran pada Liquid Burner

$$\begin{aligned} \text{AFR} &= \frac{\text{kg udara}}{\text{kg bahan bakar}} \\ &= \frac{28,00 \text{ kg}}{1,75 \text{ kg}} \\ &= 16 : 1 \end{aligned}$$

$$\begin{aligned} \text{-Mol N}_2 \text{ dari udara suplai} &= \frac{79}{100} \times \text{Mol udara total} \\ &= \frac{79}{100} \times 0,9709 \text{ kmol} \\ &= 0,7670 \text{ kmol} \\ &= 21,48 \text{ kg} \end{aligned}$$

$$\begin{aligned} \text{-Mol O}_2 \text{ dari udara suplai} &= \frac{21}{100} \times \text{Mol udara total} \\ &= \frac{21}{100} \times 0,9709 \text{ kmol} \\ &= 0,2039 \text{ kmol} \\ &= 6,52 \text{ kg} \end{aligned}$$

% N ₂ pada flue gas sama dengan % N ₂ dari udara	82,24%
Mol N ₂ pada flue gas sama dengan N ₂ dari udara	0,7670 kmol

$$\begin{aligned} \text{Mol total dry flue gas} &= \frac{100\%}{82,24\%} \times \text{-Mol N}_2 \text{ dari udara suplai} \\ &= \frac{100\%}{82,24\%} \times 0,7670 \text{ kmol} \end{aligned}$$

$$= 82,24\% \\ = 0,9326 \text{ kmol}$$

Tabel.24 komposisi dry flue gas (orsat)

Komponen	%(vol)	Mol (Kmol)	BM	Massa (Kg)
CO ₂	8,48%	0,0791	44	3,4798
CO	2,13%	0,0199	28	0,5562
O ₂	7,15%	0,0667	32	2,1338
N ₂	82,24%	0,7670	28	21,4757
Total	100,00%	0,9326		27,6456

- Menghitung H₂O pada udara

$$T \text{ dry} = 32 \text{ } ^\circ\text{C}$$

$$RH = 65\%$$

-Dari grafik humidity chart didapatkan nilai H = 0,024

$$\begin{aligned} \text{H}_2\text{O udara} &= H \times \text{Udara Suplai} \\ &= 0,024 \times 0,971 \text{ kmol} \\ &= 0,0233 \text{ kmol} \\ &= 0,4194 \text{ kg} \end{aligned}$$

- Menghitung H₂O hasil reaksi

Mol O₂ yang bereaksi pada proses pembakaran

Mol O₂ dari udara - (Mol O₂ dalam CO₂ + Mol O₂ dalam CO)

$$\begin{aligned} &0,2039 \text{ kmol} - 0,0791 \text{ kmol} + 0,0099 \text{ kmol} \\ &0,1149 \text{ kmol} \end{aligned}$$

$$\text{Mol H}_2\text{O hasil reaksi pembakaran} = 0,1149 \text{ kmol} \text{ atau } 2,0676 \text{ kg}$$

- H₂O total dalam flue gas

H₂O dari udara + H₂O hasil reaksi pembakaran

$$\begin{aligned} &0,0233 \text{ kmol} + 0,1149 \text{ kmol} \\ &0,1382 \text{ kmol} \\ &2,5238 \text{ kg} \end{aligned}$$

Tabel 25 Komposisi wet flue gas

Komponen	Massa (Kg)	BM	Mol (Kmol)
CO ₂	3,4798	44	0,0791
CO	0,5562	28	0,0199
O ₂	2,1338	32	0,0667
N ₂	21,4757	28	0,7670
H ₂ O	2,5238	18	0,1402
Total	30,1694		1,0728

Tabel 26 Komposisi udara suplai dengan humiditas

Komponen	Massa (Kg)	BM	Mol (Kmol)
O ₂	6,5243	32	0,2039
N ₂	21,4757	28	0,7670
H ₂ O	0,4194	18	0,0233
Total	28,4194		0,9942

-Sehingga didapatkan Neraca Massa

Tabel 27 Nerca Massa Sputar Boiler

INPUT		OUTPUT	
Komponen	Massa (kg)	Komponen	Massa (kg)
O ₂	6,5243	O ₂	2,1338
N ₂	21,4757	N ₂	21,4757
H ₂ O	0,4194	H ₂ O	2,5238
Solar	1,750	CO ₂	3,4798
-	-	CO	0,5562
Total	30,1694		30,1694

Neraca Energi Water Tube Boiler

INPUT

Basis 1 jam

Pada Tekanan 5 Bar

1) Menghitung Entalpi Solar

$$\begin{aligned}
 \text{Massa Solar (m}_{bb}\text{)} &= 1,75 \text{ kg} \\
 T_{\text{referensi}} &= 25 \text{ }^{\circ}\text{C} = 298 \text{ K} \\
 T_{\text{solar}} &= 30 \text{ }^{\circ}\text{C} = 303 \text{ K} \\
 \text{ }^{\circ}\text{API} &= 40 \text{ }^{\circ}\text{F} \quad (\text{Sumber : Willcox, Diesel Technology hal 304}) \\
 \text{pada Fig.66, Hougén hal 266 pada } \text{ }^{\circ}\text{API } 40 \text{ }^{\circ}\text{F} \text{ didapat cp} &= 0,502 \text{ Kcal/Kg}^{\circ}\text{C} \\
 Q_{\text{solar}} &= m_{\text{solar}} \times \text{cp solar} \times (T_{bb} - T_{\text{ref}}) \\
 &= 1,75 \text{ kg/jam} \times 0,502 \text{ Kcal/Kg}^{\circ}\text{C} \times (30 - 25) \text{ }^{\circ}\text{C} \\
 &= \mathbf{4,3925 \text{ kcal}}
 \end{aligned}$$

$$\begin{aligned}
 2. \text{ Heating Value Solar} &= m_{\text{solar}} \times \text{HHV}_{\text{solar}} \\
 &= 1,75 \text{ kg/jam} \times 10500 \text{ Kcal/kg} \\
 &= \mathbf{18375 \text{ kcal/jam}}
 \end{aligned}$$

3. Menghitung entalpi Udara

$$\begin{aligned}
 n_{\text{udara}} &= 0,9709 \text{ kmol} \\
 T_{\text{referensi}} &= 25 \text{ }^{\circ}\text{C} = 298 \text{ K} \\
 T_{\text{udara}} &= 30 \text{ }^{\circ}\text{C} = 303 \text{ K} \\
 \text{Dari Tabel 17, Hougén hal. 255 diperoleh :} \\
 a &= 6,386 \\
 b &= 0,001762 \\
 c &= -2,656\text{E-}07
 \end{aligned}$$

$$\begin{aligned}
 C_p &= a + bT + cT^2 \quad (\text{Eq.21, Hougén hal 253}) \\
 &= a + \frac{b}{2} (T_2 + T_1) + \frac{c}{3} (T_2^2 + T_2 T_1 + T_1^2) \quad (\text{Eq.25, Hougén hal 258})
 \end{aligned}$$

Maka,

$$\begin{aligned}
 C_p_{\text{udara}} &= 6,386 + \frac{0,001762}{2} \cdot 601 \text{ K} + \frac{-2,656\text{E-}07}{3} \cdot 270907 \text{ K} \\
 &= 6,891497 \text{ Kcal/Kmol.K}
 \end{aligned}$$

$$\begin{aligned}
 Q &= n \times c_p \times \Delta T \\
 &= 0,97 \cdot 6,89 \text{ Kcal/Kmol.K} \cdot 5 \text{ K} \\
 &= \mathbf{33,45 \text{ kcal}}
 \end{aligned}$$

4. Menghitung Entalpi BFW

$$\begin{aligned}
 m_{\text{Fresh Water}} &= 30 \text{ kg} \\
 T_{\text{referensi}} &= 25 \text{ }^{\circ}\text{C} = 298 \text{ K} \\
 T_{Bfw} &= 28 \text{ }^{\circ}\text{C}
 \end{aligned}$$

Dari Tabel *Properties of Saturated Water (Liquid-Vapor)*, maka nilai entalpi dari *saturated steam* saat $T = 28\text{ }^{\circ}\text{C}$ adalah 117,43 KJ/kg

$$h_f = 117,43 \text{ KJ/kg}$$

(Sumber : Moran, *Fundamentals of Engineering Thermodynamics* (2006))

$$h_f = 117,43 \text{ KJ/kg} \times 0,24 \text{ Kcal/kj}$$

$$= 28,1832 \text{ Kcal/kg}$$

Maka,

$$\begin{aligned} Q &= m_{\text{BFW}} \times h_f \\ &= 30 \text{ kg} \times 28,1832 \text{ kcal/kg} \\ &= \mathbf{845,496 \text{ kcal}} \end{aligned}$$

5. Menghitung Entalpi H₂O dari Udara

Panas laten H₂O dalam flue gas

$$h_f \text{ Pada } 30\text{ }^{\circ}\text{C} = 125,79 \text{ kj/kg}$$

$$H_{fg} = 125,79 \text{ KJ/kg}$$

$$= 125,79 \text{ KJ/kg} \times 0,24 \text{ kkal/kj}$$

$$= 30,1896 \text{ kcal/kg}$$

(Sumber : Hougen hal 236)

Entalpi uap air dalam flue gas

$$= \text{massa H}_2\text{O dalam flue gas} \times H_{fg}$$

$$= 0,4194175 \text{ kg} \times 30,1896 \text{ kcal/kg}$$

$$= \mathbf{12,66204583 \text{ kcal}}$$

OUTPUT

1) Menghitung Entalpi *Dry Flue Gas*

0

Tabel 28 Komposisi Mol Flue Gas Kering

Komponen	n (kmol)
CO ₂	0,0791
CO	0,0199
O ₂	0,0667
N ₂	0,7670
Total	0,9326

Tabel 29 Konstanta Kapasitas Panas

Komponen	A	B x 10 ⁻³	C x 10 ⁻⁶
CO ₂	6,339	10,14	-3,415
CO	6,35	1,811	-0,2675
O ₂	6,117	3,167	-1,005
N ₂	6,457	1,389	-0,069

(Sumber : Hougen, hal 255)

Kapasitas panas (C_p) tersebut dihitung dengan persamaan berikut :

$$C_p = a + \frac{b}{2} (T_2 + T_1) + \frac{c}{3} (T_2^2 + T_2 T_1 + T_1^2)$$

(Eq.25, Hougen hal 258)

$$T_{\text{referensi}} = 25 \text{ } ^\circ\text{C} = 298 \text{ K}$$

$$T_{\text{udara}} = 219 \text{ } ^\circ\text{C} = 492 \text{ K}$$

$$\Delta T = T_2 - T_1$$

$$= 194 \text{ K}$$

Maka,

$$C_p \text{ CO}_2 = 6,339 + \frac{0,01014}{2} 790 \text{ K} + \frac{0,000003415}{3} 477484 \text{ K}$$

$$= 9,800764047 \text{ Kcal/Kmol.K}$$

$$C_p \text{ CO} = 6,35 + \frac{0,001811}{2} 790 \text{ K} + \frac{-2,675\text{E-}07}{3} 477484 \text{ K}$$

$$= 7,022769343 \text{ Kcal/Kmol.K}$$

$$C_p \text{ O}_2 = 6,117 + \frac{0,003167}{2} 790 \text{ K} + \frac{0,000001005}{3} 477484 \text{ K}$$

$$= 7,20800786 \text{ Kcal/Kmol.K}$$

$$C_p \text{ N}_2 = 6,457 + \frac{0,001389}{2} 790 \text{ K} + \frac{0,000000069}{3} 477484 \text{ K}$$

$$= 6,994672868 \text{ Kcal/Kmol.K}$$

$$C_p \text{ N}_2 = 7,136 + \frac{0,00264}{2} 790 \text{ K} + \frac{4,59\text{E-}08}{3} 477484 \text{ K}$$

$$= 8,186105505 \text{ Kcal/Kmol.K}$$

Tabel 30 Konstanta Kapasitas Panas

Komponen	A	B x10 ⁻³	C x 10 ⁻⁶	Cp (Kcal/kmol.K)
CO ₂	6,339	10,14	-3,415	9,8008
CO	6,350	1,811	-0,2675	7,0228
O ₂	6,117	3,167	-1,005	7,2080

H ₂ O	7,136	2,64	0,0459	8,1861
N ₂	6,457	1,389	-0,069	6,9947

Sehingga,

$$\begin{aligned}
 Q_{\text{CO}_2} &= n_{\text{CO}_2} \times C_p_{\text{CO}_2} \times \Delta T \\
 &= 0,0791 \text{ kmol} \times 9,800764 \text{ Kcal/Kmol.K} \times 194 \text{ K} \\
 &= \mathbf{150,371067 \text{ kcal}}
 \end{aligned}$$

Tabel 31 Panas Sensibel Flue Gas

Komponen	n (kmol)	Cp	ΔT	Q
		(Kcal/kmol.K)	K	Kcal
CO ₂	0,0791	9,8008	194	150,3711
CO	0,0199	7,0228	194	27,0643
O ₂	0,0667	7,2080	194	93,2459
H ₂ O	0,0233	8,1861	194	37,0044
N ₂	0,7670	6,9947	194	1040,7802
Total	0,9559			1348,4658

2) Menghitung panas penguapan H₂O Flue Gas

Panas laten H₂O dalam flue gas

$$\begin{aligned}
 h_f &\text{ pada } 219^\circ\text{C} = 1870 \text{ kJ/kg} \\
 H_{fg} &= 1870 \text{ KJ/kg} \quad (\text{Sumber : Hougen hal 236}) \\
 &= 1870 \text{ KJ/kg} \times 0,24 \text{ kkal/kj} \\
 &= 448,8 \text{ kcal/kg}
 \end{aligned}$$

$$\begin{aligned}
 \text{Entalpi uap air dalam flue gas} &= \text{massa H}_2\text{O dalam flue gas} \times H_{fg} \\
 &= 2,5237784 \text{ kg} \times 448,8 \text{ kcal/kg} \\
 &= \mathbf{1132,671763 \text{ kcal}}
 \end{aligned}$$

$$\begin{aligned}
 \text{Jadi total entalpi flue gas} &= \text{Panas Penguapan H}_2\text{O} + \text{Entalpi Dry Flue Gas} \\
 &= 1132,67 \text{ kcal} + 1348,4658 \\
 \text{Heatloss Flue Gas} &= \mathbf{2481,1 \text{ kcal}}
 \end{aligned}$$

3) Heating Value CO Tak Terbakar

$$\begin{aligned}
 DH^{\circ}\text{c CO} &= 67000 \text{ Kcal/kmol} \\
 n_{\text{CO}} &= 0,0199 \text{ Kmol} \\
 &= 19,8649 \text{ mol}
 \end{aligned}$$

(Sumber : Tabel 30, Hougen hal 262)

Maka,

$$\begin{aligned} \text{HV CO tak terbakar} &= 67000 \text{ Kcal/mol} \quad \times \quad 0,0199 \text{ kmol} \\ &= \mathbf{1330,9483 \text{ Kcal/kmol}} \end{aligned}$$

4) Entalpi dari Saturated Steam

$$m_{\text{steam}} = 10 \text{ kg}$$

$$P_{\text{steam}} = 5 \text{ bar}$$

$$h_g = 2748,70 \text{ kJ/kg}$$

(Sumber : Moran, *Fundamentals of Engineering Thermodynamics* (2006))

$$= 2748,70 \text{ KJ/kg} \quad \times \quad 0,24 \text{ kkal/kj}$$

$$= 659,688 \text{ Kcal/kg}$$

Maka,

$$\begin{aligned} Q_{\text{Steam}} &= m_{\text{steam}} \quad \times \quad h_g \\ &= 10 \text{ kg} \quad \times \quad 659,69 \text{ Kcal/kg} \\ &= \mathbf{6596,88 \text{ Kcal}} \end{aligned}$$

5) Entalpi Blowdown

$$m_{\text{blowdown}} = 20 \text{ kg}$$

$$T_{\text{blowdown}} = 100 \text{ } ^\circ\text{C}$$

$$\text{Maka } h_f = 419,04 \text{ kJ/kg}$$

$$\begin{aligned} Q_{\text{blowdown}} &= m_{\text{blowdown}} \quad \times \quad h_f \\ &= 20 \text{ kg} \quad \times \quad 419,04 \text{ kJ/kg} \end{aligned}$$

$$= 8380,8 \text{ kJ}$$

$$= 8380,8 \text{ kJ} \quad \times \quad 0,24 \text{ kkal/kj}$$

$$= \mathbf{2011,4 \text{ kcal}}$$

6) Menghitung Heat Loss Radiasi Permukaan Furnace

$$Q = \varepsilon \cdot \Sigma \cdot A_{\text{boiler}} \left((T_s^4)/1000 - (T_{\text{ref}}^4)/1000 \right)$$

(Sumber, *Holman*. Hal 351)

Keterangan

$$Q = \text{panas radiasi}$$

$$\varepsilon = \text{emisivitas steel oxidized} = 0,78$$

$$\sigma = \text{nilai tetapan Stefan-Boltzman} = 5,67 \times 10^{-8} \text{ W/m}^2\text{K}$$

$$A = \text{luas permukaan boiler} = 2,8 \text{ m}^2$$

$$T_s = \text{temperatur dinding boiler} = 150 \text{ } ^\circ\text{C} = 423 \text{ K}$$

$$T_{\text{ref}} = \text{temperatur lingkungan} = 25 \text{ } ^\circ\text{C} = 298 \text{ K}$$

$$\begin{aligned} Q &= \varepsilon \cdot \Sigma \cdot A_{\text{boiler}} \left((T_s^4)/1000 - (T_{\text{ref}}^4)/1000 \right) \\ &= 0,78 \quad \times \quad 5,67 \times 10^{-8} \quad \times \quad 2,8 \quad \times \quad \left[(423)^4 \right] - \left[(298)^4 \right] \\ &= 2988,0157 \text{ W} \\ &= 10756,86 \text{ KJ/jam} \quad \times \quad 0,24 \text{ Kcal/Kj} \\ &= \mathbf{2581,64556 \text{ Kcal/jam}} \end{aligned}$$

7) Menghitung Heat Loss Konveksi dari permukaan Furnace

$$\begin{aligned}
 T_{\text{dinding luar}} &= 150 \text{ } ^\circ\text{C} = 423 \text{ K} \\
 T_{\text{ref}} &= 25 \text{ } ^\circ\text{C} = 298 \text{ K} \\
 \Delta T &= 125 \text{ } ^\circ\text{C} = 398 \text{ K} \\
 \text{Panjang} &= 100 \text{ cm} = 1 \text{ m} \\
 \text{Lebar} &= 58 \text{ cm} = 0,58 \text{ m} \\
 \text{Tinggi} &= 70 \text{ cm} = 0,7 \text{ m} \\
 \text{A luas} &= 2 (p. L + p.t + L.t) \\
 &= 2 \times 0,58 \times 0,7 + 0,406 \\
 &= 3,372 \text{ m}
 \end{aligned}$$

$$\begin{aligned}
 h &= 1,42 \left(\frac{\Delta T}{L} \right)^{1/4} \\
 &= 1,42 \left(\frac{125}{1} \right)^{1/4} \\
 &= 4,74806 \text{ W/m}^2\text{ } ^\circ\text{C}
 \end{aligned}$$

(Sumber: J.P. Holman Hal.315)

$$\begin{aligned}
 Q &= h \times A \times \Delta T \quad \text{(Sumber: J.P. Holman Hal.315)} \\
 &= 4,74806 \text{ W/m}^2\text{ } ^\circ\text{C} \times 3,372 \text{ m}^2 \times 100 \text{ } ^\circ\text{C} \\
 &= 1601,04 \text{ J/s/1000(3600)} \\
 &= 5763,76 \text{ Kj/jam} \\
 &= 5763,76 \text{ Kj/jam} \times 0,24 \text{ kkal/kj} \\
 &= \mathbf{1383,3} \text{ kkal/jam}
 \end{aligned}$$

Tabel 32 Neraca Energi Seputar Boiler Furnace

Komponen	Input (Kcal)	(%)	Output (Kcal)	(%)
Entalpi Solar	4,39	0,02	-	-
Heating Value Solar	18375,00	95,35	-	-
Entalpi Boiler Feed Water	845,50	4,39	-	-
Entalpi udara kering	33,45	0,17	-	-
Entalpi H2O dari Udara	12,66	0,07	-	-
Heat loss Flue Gas	-	-	2481,14	12,87
Entalpi CO yang tak terbakar	-	-	1330,95	6,91
Entalpi dari Saturated Steam	-	-	6596,88	34,23
Heatloss Blowdown	-	-	2011,39	10,44
Heat Loss Radiasi	-	-	2581,65	13,40
Heat Loss Konveksi	-	-	1383,30	7,18
Panas yang teranalisis			2885,70	14,97
Total	19271,00	100,00	19271,00	100,00

$$\text{Efisiensi Boiler Furnace} = \frac{\text{Entalpi Steam}}{\text{Total Input}} \times 100 \%$$

$$\begin{aligned} &= \frac{\text{Energi Input}}{19271,00 \text{ kcal}} \times 100 \% \\ &= \frac{6596,88 \text{ kcal}}{19271,00 \text{ kcal}} \times 100 \% \\ &= 34,23 \% \end{aligned}$$

$$\begin{aligned} \text{SEC (spesific energy consumed)} &= \frac{\text{kg bahan bakar}}{\text{kg steam}} \\ &= \frac{1,75}{10} = 0,175 \end{aligned}$$

Neraca Energi Water Tube Boiler

INPUT

Basis 1 jam

Pada Tekanan 10 Bar

1) Menghitung Entalpi Solar

$$\text{Massa Solar (m}_{bb}\text{)} = 2 \text{ kg}$$

$$T_{\text{referensi}} = 25 \text{ }^{\circ}\text{C} = 298 \text{ K}$$

$$T_{\text{solar}} = 30 \text{ }^{\circ}\text{C} = 303 \text{ K}$$

$$^{\circ}\text{API} = 40 \text{ }^{\circ}\text{F} \quad (\text{Sumber : Willcox, Diesel Technology hal 304})$$

$$\text{pada Fig.66, Hougén hal 266 pada } ^{\circ}\text{API } 40 \text{ }^{\circ}\text{F} \text{ didapat cp} = 0,502 \text{ Kcal/Kg}^{\circ}\text{C}$$

$$\begin{aligned} Q_{\text{solar}} &= m_{\text{solar}} \times \text{cp solar} \times (T_{bb} - T_{\text{ref}}) \\ &= 2 \text{ kg/jam} \times 0,502 \text{ Kcal/Kg}^{\circ}\text{C} \times (30 - 25) \text{ }^{\circ}\text{C} \\ &= \mathbf{5,02 \text{ kcal}} \end{aligned}$$

$$\begin{aligned} 2. \text{ Heating Value Solar} &= m_{\text{solar}} \times \text{HHV}_{\text{solar}} \\ &= 2 \text{ kg/jam} \times 10500 \text{ Kcal/kg} \\ &= \mathbf{21000 \text{ kcal/jam}} \end{aligned}$$

3. Menghitung entalpi Udara

$$n_{\text{udara}} = 0,9709 \text{ kmol}$$

$$T_{\text{referensi}} = 25 \text{ }^{\circ}\text{C} = 298 \text{ K}$$

$$T_{\text{udara}} = 30 \text{ }^{\circ}\text{C} = 303 \text{ K}$$

Dari Tabel 17, Hougén hal. 255 diperoleh :

$$a = 6,386$$

$$b = 0,001762$$

$$c = -2,656\text{E-}07$$

$$C_p = a + bT + cT^2 \quad (\text{Eq.21, Hougén hal 253})$$

$$= a + \frac{b}{2} (T_2 + T_1) + \frac{c}{3} (T_2^2 + T_2 T_1 + T_1^2) \quad (\text{Eq.25, Hougén hal 258})$$

Maka,

$$\begin{aligned} C_p_{\text{udara}} &= 6,386 + \frac{0,001762}{2} \cdot 601 \text{ K} + \frac{-2,656\text{E-}07}{3} \cdot 270907 \text{ K} \\ &= 6,891497 \text{ Kcal/Kmol.K} \end{aligned}$$

$$\begin{aligned} Q &= n \times c_p \times \Delta T \\ &= 0,97 \cdot 6,89 \text{ Kcal/Kmol.K} \cdot 5 \text{ K} \\ &= \mathbf{33,45 \text{ kcal}} \end{aligned}$$

4. Menghitung Entalpi BFW

$$m_{\text{Fresh Water}} = 30 \text{ kg}$$

$$T_{\text{referensi}} = 25 \text{ }^{\circ}\text{C} = 298 \text{ K}$$

$$T_{Bfw} = 28 \text{ }^{\circ}\text{C}$$

Dari Tabel *Properties of Saturated Water (Liquid-Vapor)*, maka nilai entalpi dari *saturated steam* saat $T = 28\text{ }^{\circ}\text{C}$ adalah 117,43 Kj/kg

$$h_f = 117,43 \text{ Kj/kg}$$

(Sumber : Moran, *Fundamentals of Engineering Thermodynamics* (2006))

$$h_f = 117,43 \text{ Kj/kg} \times 0,24 \text{ Kcal/kj}$$

$$= 28,1832 \text{ Kcal/kg}$$

Maka,

$$\begin{aligned} Q &= m_{\text{BFW}} \times h_f \\ &= 30 \text{ kg} \times 28,1832 \text{ kcal/kg} \\ &= \mathbf{845,496 \text{ kcal}} \end{aligned}$$

5. Menghitung Entalpi H₂O dari Udara

Panas laten H₂O dalam flue gas

$$h_f \text{ pada } 30\text{ }^{\circ}\text{C} = 125,79 \text{ kj/kg}$$

$$H_{fg} = 125,79 \text{ Kj/kg}$$

(Sumber : Hougen hal 236)

$$= 125,79 \text{ Kj/kg} \times 0,24 \text{ kkal/kj}$$

$$= 30,1896 \text{ kcal/kg}$$

Entalpi uap air dalam flue

$$\text{gas} = \text{massa H}_2\text{O dalam flue gas} \times H_{fg}$$

$$= 0,4194175 \text{ kg} \times 30,1896 \text{ kcal/kg}$$

$$= \mathbf{12,66204583 \text{ kcal}}$$

OUTPUT

1) Menghitung Entalpi *Dry Flue Gas*

0

Tabel 33 Komposisi Mol Flue Gas Kering

Komponen	n (kmol)
CO ₂	0,0791
CO	0,0199
O ₂	0,0667
N ₂	0,7670
Total	0,9326

Tabel 34 Konstanta Kapasitas Panas

Komponen	A	B x 10 ⁻³	C x 10 ⁻⁶
CO ₂	6,339	10,14	-3,415
CO	6,35	1,811	-0,2675
O ₂	6,117	3,167	-1,005
N ₂	6,457	1,389	-0,069

(Sumber : Hougen, hal 255)

Kapasitas panas (C_p) tersebut dihitung dengan persamaan berikut :

$$C_p = a + \frac{b}{2} (T_2 + T_1) + \frac{c}{3} (T_2^2 + T_2 T_1 + T_1^2)$$

(Eq.25, Hougen hal 258)

$$T_{\text{referensi}} = 25 \text{ } ^\circ\text{C} = 298 \text{ K}$$

$$T_{\text{udara}} = 30 \text{ } ^\circ\text{C} = 303 \text{ K}$$

$$\begin{aligned} \Delta T &= T_2 - T_1 \\ &= 5 \text{ K} \end{aligned}$$

Maka,

$$\begin{aligned} C_p \text{ CO}_2 &= 6,339 + \frac{0,01014}{2} (601 \text{ K} + 270907 \text{ K}) + \frac{0,000003415}{3} (601 \text{ K}^2 + 601 \text{ K} \cdot 270907 \text{ K} + 270907 \text{ K}^2) \\ &= 9,077687532 \text{ Kcal/Kmol.K} \end{aligned}$$

$$\begin{aligned} C_p \text{ CO} &= 6,35 + \frac{0,001811}{2} (601 \text{ K} + 270907 \text{ K}) + \frac{-2,675\text{E-}07}{3} (601 \text{ K}^2 + 601 \text{ K} \cdot 270907 \text{ K} + 270907 \text{ K}^2) \\ &= 6,870049626 \text{ Kcal/Kmol.K} \end{aligned}$$

$$\begin{aligned} C_p \text{ O}_2 &= 6,117 + \frac{0,003167}{2} (601 \text{ K} + 270907 \text{ K}) + \frac{0,000001005}{3} (601 \text{ K}^2 + 601 \text{ K} \cdot 270907 \text{ K} + 270907 \text{ K}^2) \\ &= 6,977929655 \text{ Kcal/Kmol.K} \end{aligned}$$

$$\begin{aligned} C_p \text{ N}_2 &= 6,457 + \frac{0,001389}{2} (601 \text{ K} + 270907 \text{ K}) + \frac{0,000000069}{3} (601 \text{ K}^2 + 601 \text{ K} \cdot 270907 \text{ K} + 270907 \text{ K}^2) \\ &= 6,868163639 \text{ Kcal/Kmol.K} \end{aligned}$$

$$\begin{aligned} C_p \text{ N}_2 &= 7,136 + \frac{0,00264}{2} (601 \text{ K} + 270907 \text{ K}) + \frac{4,59\text{E-}08}{3} (601 \text{ K}^2 + 601 \text{ K} \cdot 270907 \text{ K} + 270907 \text{ K}^2) \\ &= 7,933464877 \text{ Kcal/Kmol.K} \end{aligned}$$

Tabel 35 Konstanta Kapasitas Panas

Komponen	A	B x10 ⁻³	C x 10 ⁻⁶	C _p
				(Kcal/kmol.K)
CO ₂	6,339	10,14	-3,415	9,0777
CO	6,350	1,811	-0,2675	6,8700
O ₂	6,117	3,167	-1,005	6,9779

H ₂ O	7,136	2,64	0,0459	7,9335
N ₂	6,457	1,389	-0,069	6,8682

Sehingga,

$$\begin{aligned}
 Q_{\text{CO}_2} &= n_{\text{CO}_2} \times C_p_{\text{CO}_2} \times \Delta T \\
 &= 0,0791 \text{ kmol} \times 9,077688 \text{ Kcal/Kmol.K} \times 5 \text{ K} \\
 &= \mathbf{3,58961483 \text{ kcal}}
 \end{aligned}$$

Tabel 36 Panas Sensibel Flue Gas

Komponen	n (kmol)	C _p	ΔT	Q
		(Kcal/kmol.K)	K	Kcal
CO ₂	0,0791	9,0777	5	3,5896
CO	0,0199	6,8700	5	0,6824
O ₂	0,0667	6,9779	5	2,3265
H ₂ O	0,0233	7,9335	5	0,9243
N ₂	0,7670	6,8682	5	26,3391
Total	0,9559			33,8619

2) Menghitung panas penguapan H₂O Flue Gas

Panas laten H₂O dalam flue gas

$$h_f \text{ Pada } 221 \text{ }^\circ\text{C} = 2801 \text{ kJ/kg}$$

$$H_{fg} = 2801 \text{ KJ/kg} \quad (\text{Sumber : Hougen hal 236})$$

$$= 2801 \text{ KJ/kg} \times 0,24 \text{ kkal/kj}$$

$$= 672,24 \text{ kkal/kg}$$

$$\text{Entalpi uap air dalam flue gas} = \text{massa H}_2\text{O dalam flue gas} \times H_{fg}$$

$$= 2,5237784 \text{ kg} \times 672,24 \text{ kkal/kg}$$

$$= \mathbf{1696,584818 \text{ kcal}}$$

$$\text{Jadi total entalpi flue gas} = \text{Panas Penguapan H}_2\text{O} + \text{Entalpi Dry Flue Gas}$$

$$= 1696,58 \text{ kcal} + 33,8619$$

$$\text{Heatloss Flue Gas} = \mathbf{1730,4 \text{ kcal}}$$

3) Heating Value CO Tak Terbakar

$$DH^{\circ}\text{C CO} = 67000 \text{ Kcal/kmol}$$

(Sumber : Tabel 30, Hougen hal 262)

$$n_{\text{CO}} = 0,0199 \text{ Kmol}$$

$$= 19,8649 \text{ mol}$$

Maka,

$$\begin{aligned} \text{HV CO tak terbakar} &= 67000 \text{ Kcal/mol} \times 0,0199 \text{ kmol} \\ &= \mathbf{1330,9483 \text{ Kcal/kmol}} \end{aligned}$$

4) Entalpi dari Saturated Steam

$$\begin{aligned} m_{\text{steam}} &= 15 \text{ kg} \\ P_{\text{steam}} &= 10 \text{ bar} \\ h_g &= 2778,00 \text{ kJ/kg} \\ &\text{(Sumber : Moran, } \textit{Fundamentals of Engineering Thermodynamics} \text{ (2006))} \\ &= 2778,00 \text{ KJ/kg} \times 0,24 \text{ kkal/kj} \\ &= 666,72 \text{ Kcal/kg} \end{aligned}$$

Maka,

$$\begin{aligned} Q_{\text{Steam}} &= m_{\text{steam}} \times h_g \\ &= 15 \text{ kg} \times 666,72 \text{ Kcal/kg} \\ &= \mathbf{10000,8 \text{ Kcal}} \end{aligned}$$

Entalpi

5) Blowdown

$$\begin{aligned} m_{\text{blowdown}} &= 15 \text{ kg} \\ T_{\text{blowdown}} &= 100 \text{ } ^\circ\text{C} \\ \text{Maka } h_f &= 419,04 \text{ kJ/kg} \\ Q_{\text{blowdown}} &= m_{\text{blowdown}} \times h_f \\ &= 15 \text{ kg} \times 419,04 \text{ kJ/kg} \\ &= 6285,6 \text{ kJ} \\ &= 6285,6 \text{ kJ} \times 0,24 \text{ kkal/kj} \\ &= \mathbf{1508,5 \text{ kcal}} \end{aligned}$$

6) Menghitung Heat Loss Radiasi Permukaan Furnace

$$Q = \epsilon \cdot \Sigma \cdot A_{\text{boiler}} \left((T_s^4)/1000 - (T_{\text{ref}}^4)/1000 \right) \quad \text{(Sumber, } \textit{Holman. Hal 351})$$

Keterangan

$$\begin{aligned} Q &= \text{panas radiasi} \\ \epsilon &= \text{emisivitas steel oxidized} = 0,78 \\ \sigma &= \text{nilai tetapan Stefan-Boltzman} = 5,67 \times 10^{-8} \text{ W/m}^2\text{K} \\ A &= \text{luas permukaan boiler} = 2,8 \text{ m}^2 \\ &\quad \text{temperatur dinding} \\ T_s &= \text{boiler} = 152 \text{ } ^\circ\text{C} = 425 \text{ K} \\ T_{\text{ref}} &= \text{temperatur lingkungan} = 25 \text{ } ^\circ\text{C} = 298 \text{ K} \end{aligned}$$

$$\begin{aligned} Q &= \epsilon \cdot \Sigma \cdot A_{\text{boiler}} \left((T_s^4)/1000 - (T_{\text{ref}}^4)/1000 \right) \\ &= 0,78 \times 5,67 \times 10^{-8} \times 2,8 \times \left[(425)^4 \right] - \left[(298)^4 \right] \\ &= 3063,529385 \text{ W} \\ &= 11028,71 \text{ Kj/jam} \times 0,24 \text{ Kcal/Kj} \\ &= \mathbf{2646,88939 \text{ Kcal/jam}} \end{aligned}$$

7) Menghitung Heat Loss Konveksi dari permukaan Furnace

$$\begin{aligned}
 T_{\text{dinding luar}} &= 152 \text{ } ^\circ\text{C} = 425 \text{ K} \\
 T_{\text{ref}} &= 25 \text{ } ^\circ\text{C} = 298 \text{ K} \\
 \Delta T &= 127 \text{ } ^\circ\text{C} = 400 \text{ K} \\
 \text{Panjang} &= 100 \text{ cm} = 1 \text{ m} \\
 \text{Lebar} &= 58 \text{ cm} = 0,58 \text{ m} \\
 \text{Tinggi} &= 70 \text{ cm} = 0,7 \text{ m} \\
 \text{A luas} &= 2 (p. L + p.t + L.t) \\
 &= 2 \times 0,58 + 0,7 + 0,406 \\
 &= 3,372 \text{ m}
 \end{aligned}$$

$$\begin{aligned}
 h &= 1,42 \left[\frac{\Delta T}{L} \right]^{1/4} \\
 &= 1,42 \left[\frac{127}{1} \right]^{1/4} \\
 &= 4,76694 \text{ W/m}^{2^\circ\text{C}}
 \end{aligned}$$

(Sumber: J.P. Holman Hal.315)

$$\begin{aligned}
 Q &= h \times A \times \Delta T \quad (\text{Sumber: J.P. Holman Hal.315}) \\
 &= 4,76694 \text{ W/m}^{2^\circ\text{C}} \times 3,372 \text{ m}^2 \times 100 \text{ } ^\circ\text{C} \\
 &= 1607,41 \text{ J/s/1000(3600)} \\
 &= 5786,68 \text{ Kj/jam} \\
 &= 5786,68 \text{ Kj/jam} \times 0,24 \text{ kkal/kj} \\
 &= \mathbf{1388,8} \text{ kkal/jam}
 \end{aligned}$$

Tabel 37 Neraca Energi Seputar Boiler Furnace

Komponen	Input (Kcal)	(%)	Output (Kcal)	(%)
Entalpi Solar	5,02	0,02	-	-
Heating Value Solar	21000,00	95,91	-	-
Entalpi Boiler Feed Water	845,50	3,86	-	-
Entalpi udara kering	33,45	0,15	-	-
Entalpi H2O dari Udara	12,66	0,06	-	-
Heat loss Flue Gas	-	-	1730,45	7,90
Entalpi CO yang tak terbakar	-	-	1330,95	6,08
Entalpi dari Saturated Steam	-	-	10000,80	45,67
Heatloss Blowdown	-	-	1508,54	6,89
Heat Loss Radiasi	-	-	2646,89	12,09
Heat Loss Konveksi	-	-	1388,80	6,34
Panas yang teranalisis			3290,20	15,03
Total	21896,63	100,00	21896,63	100,00

$$\begin{aligned} \text{Efisiensi Boiler Furnace} &= \frac{\text{Entalpi Steam}}{\text{Energi Input}} \times 100 \% \\ &= \frac{10000,80 \text{ kcal}}{21896,63 \text{ kcal}} \times 100 \% \\ &= 45,67 \% \end{aligned}$$

$$\begin{aligned} \text{SEC (specific energy consumed)} &= \frac{\text{kg bahan bakar}}{\text{kg steam}} \\ &= \frac{2}{15} = 0,133333333 \end{aligned}$$